A Flexible Transient Subglacial Hydrology Model

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Context

- Liquid water reaches the bed via moulins and the englacial system
- High water pressure at the bed causes increased basal sliding
- Geometry of the subglacial system evolves with water input and flow
- Subglacial hydrology may be key to understanding velocity signals and patterns that are not yet well understood



Moon et al. (2014), Geophys. Res. Let.

Overview of Model Equations

Continuity Equation (mass balance)

 $\frac{\partial b}{\partial t} +$ $\vdash \nabla \cdot \vec{q} = \frac{m}{2} - \frac{m}{2}$

b - subglacial gap height (m) \vec{q} - gap-integrated basal water flux (m²s⁻¹) \vec{m} - melt rate (m s⁻¹) ρ_w - density of water (kg m⁻³) $i_{e\rightarrow b}$ - rate of input from englacial system to subglacial system (m s⁻¹)

Basal Gap Dynamics

$$\frac{\partial b}{\partial t} = \frac{\dot{m}}{\rho_i} - A|p_i - p_w|^{n-1}(p_i - p_w)b + \beta u_b$$

- ho_i bulk density of ice (kg m⁻³)
- A flow law parameter (Pa^{-3} \rm s^{-1})
- p_i ice overburden pressure (Pa)
- p_w water pressure (Pa)
- n flow law exponent (dimensionless, taken as 3)
- β parameter controlling average basal gap increase due to sliding (dimensionless)

Basal Gap Dynamics

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$$\begin{array}{c} \text{Opening by}\\ \text{melt} \end{array} \qquad \text{Creep closure} \qquad \begin{array}{c} \text{Opening over bumps} \end{array}$$

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Basal Water Flux (approximate momentum equation)

 Permits either laminar or turbulent flow, depending on Reynolds' number

$$\vec{q} = \frac{-b^3 g}{12\nu(1+\omega Re)}\nabla h$$

- g gravitational acceleration (m s⁻²)
- ν kinematic viscosity of water at 0 degrees C (m² s^{-1})
- ω parameter controlling transition to nonlinear resistance in basal system
- Re Reynolds number, $Re = \frac{|\vec{q}|}{\nu}$ (dimensionless)

$$h$$
 - hydraulic head (m), $h = rac{p_w}{
ho_w g} + z_b$

Internal Melt Generation (energy equation)

 $\dot{m} = \frac{1}{L} (G + \vec{u}_b \cdot \vec{\tau}_b - \rho_w g \vec{q} \cdot \nabla h)$

$$L$$
 - latent heat of fusion for water (J kg⁻¹)
 G - geothermal flux (W m⁻²)
 \vec{e} - basel treation

Internal Melt Generation (energy equation)



L - latent heat of fusion for water (J kg⁻¹) G - geothermal flux (W m⁻²) $\vec{\tau}_b$ - basal traction Combine the previous equations to form a nonlinear elliptic PDE in terms of hydraulic head (*h*):

$$rac{\partial}{\partial x} [rac{-b^3 g}{12
u (1+\omega Re)} rac{\partial h}{\partial x}] + rac{\partial}{\partial y} [rac{-b^3 g}{12
u (1+\omega Re)} rac{\partial h}{\partial y}] =$$

$$\dot{m}(\frac{1}{\rho_w} - \frac{1}{\rho_i}) + A|p_i - p_w|^{n-1}(p_i - p_w)b - \beta u_b + i_{e \to b}$$

$$h$$
 - hydraulic head (m), $h = rac{p_w}{
ho_w g} + z_b$

Model Description

Use a Picard iteration within each time-step to solve the elliptic PDE for the head distribution - handles the nonlinearity of Reynolds' number (*Re*) and flux (*q*), as well as RHS terms that depend on *h*

Explicitly update the gap height geometry (b) from $\frac{\partial b}{\partial t}$ equation

Model Description

- Currently implemented as a stand-alone model in MATLAB and in the Ice Sheet System Model (ISSM)
- 2D finite element and finite volume formulations

- Channels are not prescribed or treated differently than the rest of the domain; they grow and decay naturally, as does any other gap geometry
- Can handle transient water inputs (seasonal, diurnal cycles)

Case 1 – Single Moulin

- 1km x 1km square domain
- 300m-thick tilted slab
- Dirichlet boundary condition on right edge (atmospheric pressure), Neumann no-flux condition on top, left, bottom boundaries
- Constant uniform input from englacial system
- Single moulin at center of domain with diurnally-varying input for 90 days, time-step of 3 hours



Subglacial gap height evolution (m)



Case 2 - Effect of Ice Thickness

- No englacial input
- Diurnal moulin input at center (nonphysical sinusoidal input with maximum 2.5 m³ s⁻¹)

Amplitude of head fluctuations depends on ice thickness (with same input, thicker ice = larger head fluctuations)

Note that this type of sinusoidal moulin input is not physically realistic, but should be a coupled system related to storage.



Case 3 – Moulin and Boundary Inflow

- Same as Case 1, but now with diurnally-varying inflow at left boundary (non-zero Neumann condition) from y=400 to 600m
- Useful capability for simulating only part of a drainage domain

Subglacial Gap Height (m)



Hydraulic Head (m)



Case 4 - Multiple Moulins

Same as Case 1, but with 4 moulins with diurnally-varying input at (x=500, y=500), (x=300, y=700), (x=250, y=300), and (x=750, y=600)



Case 5 – Single Moulin, Steady Input: Effect of Opening by Sliding

• Similar to Case 1, but with steady moulin input at center and thicker ice (500m-thick slab)



Upcoming Plans

- Two-way coupling with ice dynamics: coupling occurs between water pressure and sliding velocity (incorporate into ISSM, CISM, MPAS-LI)
- Numerical experiments on realistic domains with realistic input forcing, with the objective of understanding and explaining the distinctly different seasonal velocity signals observed in outlet glaciers in different regions of the Greenland ice sheet

Thank you.

Question, comments, thoughts, ideas? aleah.sommers@colorado.edu